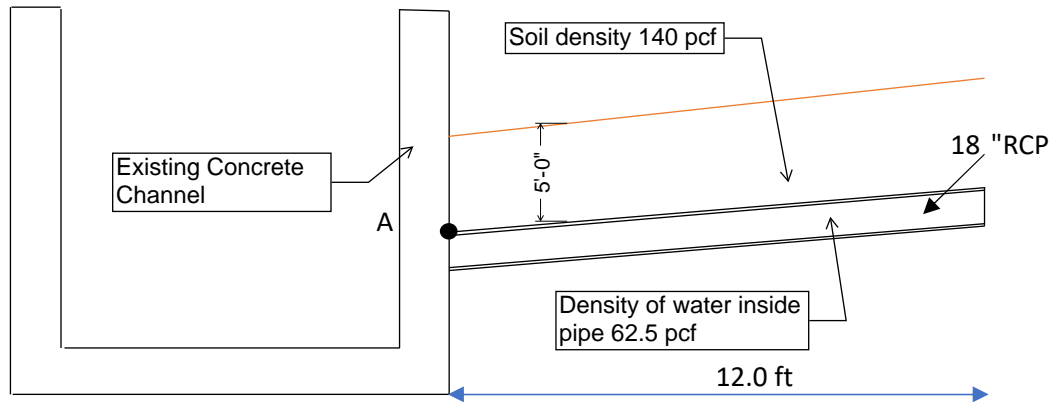


THE REINFORCED CONCRETE COLLAR ANALYSIS



A. Design Critia

1/ Code References

- a - EM 1110-2-2014
- b - EM 1110-2-2100
- c - EM 1110-2-2007
- e - EM 1110-2-2502
- d - EM 1110-2-2902
- f - Concrete Pipe Design Manual, American Concrete Pipe Association
- g - Design Data , Highway Live load on Concrete Pipe, American Concrete Pipe Association

2/ Loading

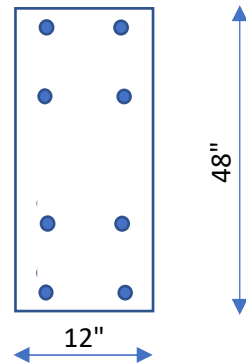
For 18 inch RCP(D-Load 2500) located at 5ft from the finished grade

Pipe outter diameter	$D_i =$	1.5 ft	
Pipe outter diameter	$D =$	2 ft	
Pipe Length	$L =$	12 ft	
Soil height above pipe	$h =$	5 ft	
Soil density	$g =$	140 pcf	
Pipe self weight	$w_p =$	168 lb/ft	
soil above pipe	$w_s =$	1400 lb/ft	
Full water in pipe	$w_w =$	110 lb/ft	
Load combination			
Load factor	$LF =$	2.2	(3-2, EM-1100-2-2014)
$U = LF*(Lp + Ltu + Ldu)$	$U =$	3692 lb/ft	
	$U = 2.2*(168 + 1400 + 110)$		

B. Shear and Moment

Moment at collar	$M =$	266 k-ft
Shear at collar	$V =$	44 kips

C. Analysis of collar connection



$$\begin{aligned} \beta_1 &= 0.85 \\ f'_c &= 4 \text{ ksi} \\ f_y &= 60 \text{ ksi} \\ E_s &= 29000 \text{ ksi} \\ d &= 12 \text{ in} \\ b &= 48 \text{ in} \\ A_s &= 1.24 \text{ in}^2 \end{aligned}$$

a. Steel ratio

$$\rho_{act} = A_s / (b * d)$$

$$\rho_b = 0.85 * b_1 * f'_c / f_y$$

$$\rho_{act} = 0.00215$$

$$\rho_b = 0.02851$$

$$\rho_{act} = 0.00215 < 0.25 * \rho_b = 0.0071$$

=> The detailed analyses of the serviceability limit states are not required

b. Compute the flexural capacity

rebar cover

$$\begin{aligned} c &= 2 \\ \phi &= 0.85 \\ a &= 0.455882353 \text{ in.} \end{aligned}$$

$$\phi M_n = f * A_s * f_y (d - a / 2)$$

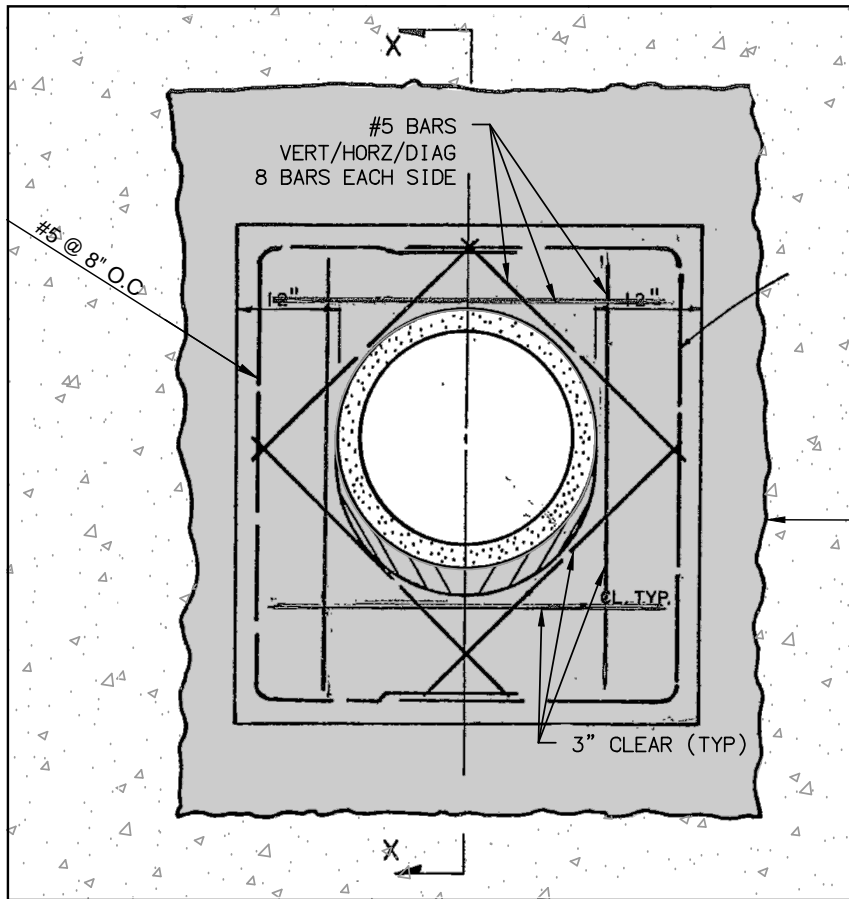
$$\phi M_n = 617.99 \text{ k-ft} > 266 \text{ :OK}$$

c. Check Shear

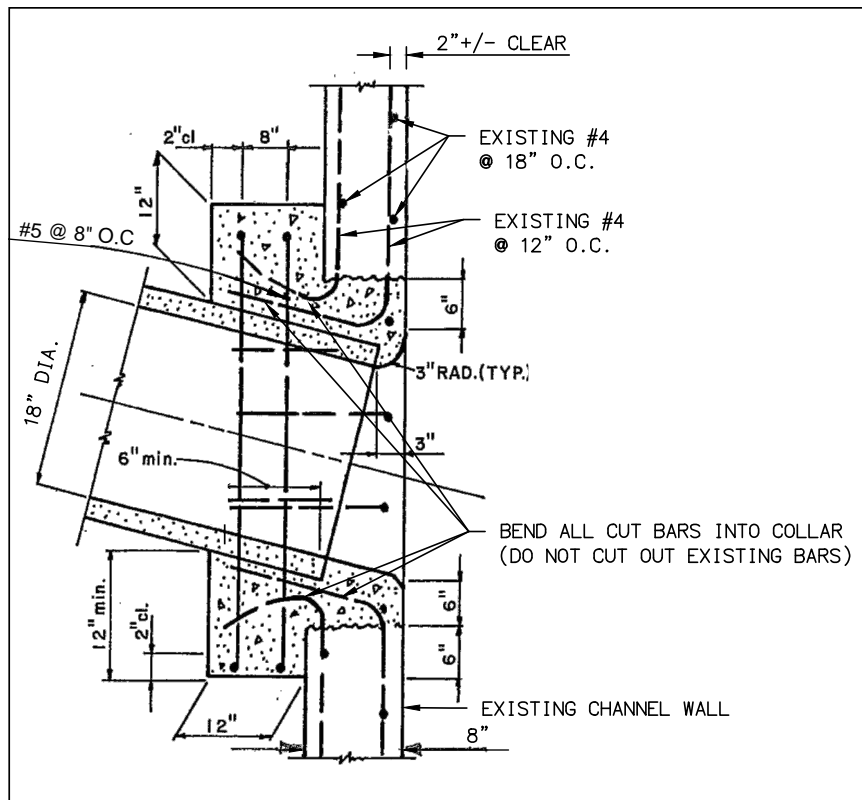
$$V_c = 2 \sqrt{f'_c} * b * d$$

$$\phi = 0.85$$

$$\phi V_c = 1728 \text{ kips} > 44 \text{ :OK}$$



ELEVATION



SECTION X-X

D-Load Calculations For The Proposed 18-in RCP Side Drain.

DESCRIPTION

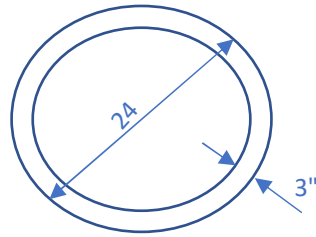
D-Load calculation were per formed for a 18" RCP being punched through the existing retaining wall

FIGURES

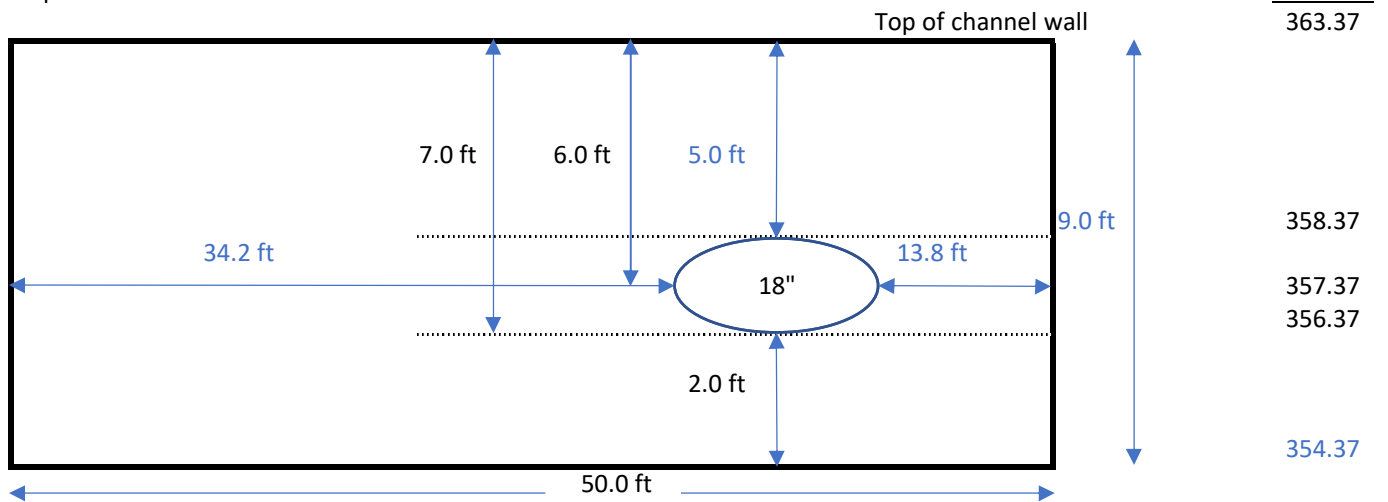
All measurements in feet unless specified otherwise

Actual pipe dimensions

(considering 11.7% vertical slope noted on HDR plans CD00006)



Top channel wall section



D-LOAD

Pipe properties

Internal pipe diameter

$D_i = 1.5$ ft

pipe thickness

$t = 0.25$ ft

soil unit weight

$\gamma_s = 140$ pcf

Height of fill above conduit

$H = 5$ ft

Factor of safety

$FS = 1.25$ (Storm drains)

Loads

Soil friction coefficient

$K_u' = 0.15$ (for trench condition)

Trench width

$B_d = 4$ ft

Trench coefficient

$C_d = 1.04$

$$C_d = \frac{1 - e^{-2K_u' \frac{H}{B_d}}}{2K_u'}$$

(base width of pipe +12" on each side per Flood Control District plans)

Earth load

$W_e = 2334.91$

$$W_e = C_d \gamma B_d^2$$

Live load

$W_l = 0$

Total vertical load

$W = 2334.91$

Load factor

Load factor for trench condition
(case 3 bedding installation)

$L.F. = 2.7$

D-Load

$$D - load = \frac{W \times S.F.}{D_i \times L.F.} \qquad \text{D-Load} = \qquad 720.65$$

Rounding factor

For pipes 36" and less in diameter, round the calculated D-Load value to the next highest 250

$$\text{D-Load}_{0.01} = \qquad \qquad \qquad \mathbf{750 \text{ lb}}$$